

**IECON 2022** 48<sup>th</sup> Annual Conference of the IEEE Industrial Electronics Society October 17-20 ,2022 | Brussels

#### **Use of Resonant Terms in a 2DOF Control** Scheme for the Current Control of an **Active Power Filter**

Fco. Javier López Alcolea<sup>1</sup>, Emilio J. Molina-Martínez<sup>1</sup>, Javier Vázquez<sup>1</sup>, Pedro Roncero-Sánchez<sup>1</sup>, Alfonso Parreño Torres<sup>2</sup>, Ismael Payo<sup>3</sup>

<sup>1</sup> Institute of Energy Research and Industrial Applications, UCLM <sup>2</sup> School of Industrial Engineering of Albacete, UCLM <sup>3</sup> Institute of Industrial and Aerospace Engineering, UCLM



















**TÉCNICO** 

2

IECON 2022 48<sup>th</sup> Annual Conference of the IEEE Industrial Electronics Society October 17-20,2022 | Brussels

# Index

- 1. Introduction
- 2. System Description
- 3. Design of the Control Stage

November of the

UCLM

- 4. Design Example
- 5. Simulation Results
- 6. Conclusions





Consejeria de la Priniderata, Administración Pública e Interior Conservería de Matteriola y Piranti existe Fac

de Andalucia

100 1 000



# 1. Introduction

- Number of non-linear and single-phase loads has increased
- Current harmonics
- Voltage and current disbalances
- Power quality issues
- Reduction of the power transferred in the grid
- EMC issues
- Shunt Active Power Filter (APF)
- Current disturbances: e.g., Current harmonics and disbalances
- Reactive Power





# 1. Introduction

- Operation of the APF: 3 different Stages
- Extraction of the undesired current components
- Control of the APF
- PWM modulation
- Objective: Control stage of an APF with an LCL filter placed at its output
- Control scheme based on a 2-Degrees-of-Freedom (2DOF) structure
- Damping of the LCL filter
- Independent control of each phase of the APF
  - $\circ~$  Can be also applied to single-phase systems
  - $\circ~$  Use of a Synchronous Reference Frame (SRF) for control purposes is avoided





### 2. System Description







### 2. System Description







# 2. System Description

- LCL Filter Model
  - Single-phase model of the LCL filter
    - Neglecting magnetizing inductance of the transformer











• 2DOF Controller



$$R_d(z) = R_\omega(z) \cdot R_p(z)$$

$$R_\omega(z) = \frac{R_{\omega,n}(z)}{R_{\omega,d}(z)} = \frac{z-1}{z^2 + c_0 z + 1}$$

$$c_0 = -2\cos(2\pi f_0 T_s)$$

$$R_p(z) = \frac{R_{p,n}(z)}{R_{p,d}(z)} = \frac{K_1 z - K_0}{z^3 + \rho_2 z^2 + \rho_1 z + \rho_0}$$

$$R_f(z) = \frac{R_{p,n}(z)}{R_{p,d}(z)} = \frac{K_5 z^3 - K_4 z^2 + K_3 z + K_2}{z^3 + \rho_2 z^2 + \rho_1 z + \rho_0}$$





• 2DOF Controller



$$H(z) = \frac{N(z)}{F(z)}$$

$$F(z) = P_d(z)R_{\omega,n}(z)R_{p,n}(z) +$$

$$+ P_n(z)[R_{p,n}(z)R_{\omega,n}(z) + R_{2,n}(z)R_{\omega,d}(z)]$$

$$F(z) = (z - p_9) \dots (z - p_0)$$
System of linear equations







$$R_h(z) = \frac{1}{z^2 + c_h z + 1} \cdot k_h \frac{z - \beta_h}{z - \alpha_h}$$

$$c_h = -2\cos(2\pi h f_0 T_s)$$

Particular solution:

 $\alpha_h = 0$ 



#### LCL Filter

| Parameter     | Value      | Parameter               | Value |
|---------------|------------|-------------------------|-------|
| $L_f(mH)$     | 2.6        | $R_{Lf}$ (m $\Omega$ )  | 80    |
| $C_f(\mu F)$  | 46         | $R_{Cf}(m\Omega)$       | 50    |
| $L_{d1}(mH)$  | 0.155      | $R_{Ld1}$ (m $\Omega$ ) | 200   |
| $L_{d2}$ (mH) | 0.274      | $R_{Ld1}$ (m $\Omega$ ) | 300   |
| r             | $\sqrt{3}$ | $T_s (\mu s)$           | 100   |

#### Location of the Poles

| Pole  | Location | Pole  | Location |
|-------|----------|-------|----------|
| $p_0$ | 0.966    | $p_5$ | 0        |
| $p_1$ | 0.966    | $p_6$ | 0        |
| $p_2$ | -0.2826  | $p_7$ | 0        |
| $p_3$ | 0.483    | $p_8$ | 0        |
| $p_4$ | 0.483    |       |          |



#### LCL Filter

| Parameter     | Value      | Parameter               | Value |
|---------------|------------|-------------------------|-------|
| $L_f(mH)$     | 2.6        | $R_{Lf}$ (m $\Omega$ )  | 80    |
| $C_f(\mu F)$  | 46         | $R_{Cf}(m\Omega)$       | 50    |
| $L_{d1}(mH)$  | 0.155      | $R_{Ld1}(m\Omega)$      | 200   |
| $L_{d2}$ (mH) | 0.274      | $R_{Ld1}$ (m $\Omega$ ) | 300   |
| r             | $\sqrt{3}$ | $T_s(\mu s)$            | 100   |

#### **Control Parameters**

| Param.                | Value    | Param.                | Value   |
|-----------------------|----------|-----------------------|---------|
| C <sub>0</sub>        | -1.9990  | $ ho_0$               | 0.1597  |
| $ ho_1$               | 0.9207   | $ ho_2$               | 1.4122  |
| <i>K</i> <sub>0</sub> | -3.2085  | <i>K</i> <sub>1</sub> | 3.9929  |
| <i>K</i> <sub>2</sub> | -3.2085  | <i>K</i> <sub>3</sub> | 31.4209 |
| $K_4$                 | -19.8707 | <i>K</i> <sub>5</sub> | 4.1270  |





#### Control Parameters

|   |                |                | COMPANIES I            |
|---|----------------|----------------|------------------------|
| h | c <sub>h</sub> | k <sub>h</sub> | $\boldsymbol{\beta}_h$ |
| 3 | -1.9911        | 0.280          | 0.800                  |
| 5 | -1.9754        | 0.260          | 0.850                  |
| 7 | -1.9518        | 0.255          | 0.930                  |
| 9 | -1.9206        | 0.230          | 0.975                  |















### 5. Simulation results

- Hardware-In-the-Loop (HIL) Emulation
  - Typhoon HIL 402 & dSPACE MicroLabBox
- Three Loads
  - Load A
    - $\circ$   $\,$  Positive, negative and zero sequence components
    - $\circ~$  5 A, 4 A and 2 A RMS, respectively
  - Load B
    - $\circ~$  Inductive load: L = 20 mH, R = 62  $\Omega$
  - Load C

| h | Amplitude | $\hat{l}_{h}/\hat{l}_{1}$ (%) | h | Amplitude | $\hat{I}_h / \hat{I}_1 (\%)$ |
|---|-----------|-------------------------------|---|-----------|------------------------------|
| 1 | 20        | -                             | 7 | 1.44      | 7.2                          |
| 3 | 4.32      | 21.6                          | 9 | 0.76      | 3.8                          |
| 5 | 2.14      | 10.7                          |   |           |                              |





### 5. Simulation results







### 5. Simulation results





### 6. Conclusions

- Current control for a three-phase four-wire APF with an LCL filter
- Damping of the LCL filter
- Can be also applied to single-phase systems
- Control scheme based on a 2D0F structure
- 2DOF controller for tracking the 50 Hz signal
- Resonant regulators for tracking harmonic components
- Simulation results
- Fast tracking of the 50 Hz signal (2D0F controller)
- Proper tracking and compensation of the current harmonics





### 6. Conclusions

• Future work: Experimental results





### 6. Conclusions

• Future work: Experimental results





**IECON 2022** 48<sup>th</sup> Annual Conference of the **IEEE Industrial Electronics Society** October 17-20 ,2022 | Brussels

# Thank you for your attention!



This work was supported by the European Regional Development Fund (ERDF) under the program Interreg SUDOE SOE3/P3/E0901 (Project: IMPROVEMENT).

UCLM













Consejería de la Presidencia, Administración Pública e Interior Consejería de Hacienda y Financiación Europe:

